

Energy-Aware Trajectory Optimization for UAV-Mounted RIS and Full-Duplex Relay

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Abstract—In the evolving landscape of sixth-generation (6G) wireless networks, unmanned aerial vehicles (UAVs) have emerged as transformative tools for dynamic and adaptive connectivity. However, dynamically adjusting their position to offer favorable communication channels introduces operational challenges in terms of energy consumption, especially when integrating advanced communication technologies like reconfigurable intelligent surfaces (RISs) and full-duplex relays (FDRs). To this end, by recognizing the pivotal role of UAV mobility, this article introduces an energy-aware trajectory design for UAV-mounted RISs and UAV-mounted FDRs using the decode-and-forward (DF) protocol, aiming to maximize the network's minimum rate and enhance user fairness, while taking into consideration the available on-board energy. Specifically, this work highlights their distinct energy consumption characteristics and their associated integration challenges by developing appropriate energy consumption models for both UAV-mounted RISs and FDRs that capture the intricate relationship between key factors, such as weight and their operational characteristics. Furthermore, a joint time-division multiple access (TDMA) user scheduling-UAV trajectory optimization problem is formulated, considering the power dynamics of both systems, while assuring that the UAV energy is not depleted mid-air. Finally, simulation

results underscore the importance of energy considerations in determining the optimal trajectory and scheduling and provide insights into the performance comparison of UAV-mounted RISs and FDRs in UAV-assisted wireless networks.

Index Terms—Energy efficiency, full-duplex relay (FDR), reconfigurable intelligent surface (RIS), trajectory optimization, unmanned aerial vehicle (UAV).

I. INTRODUCTION

UNMANNED aerial vehicles (UAVs) are emerging as transformative tools in the landscape of future sixth-generation (6G) wireless networks [1], [2]. Specifically, their inherent flexibility allows them to follow optimized trajectories, dynamically adjusting their paths to offer Line-of-Sight (LoS) channels ubiquitously. This capability makes them invaluable in scenarios demanding adaptive connectivity solutions, such as bridging connectivity gaps in challenging terrains or enhancing network resilience in disaster-stricken areas [1], [3]. Furthermore, their ability to provide on-demand high-capacity coverage in crowded events or remote locations underscores their pivotal role in reshaping wireless communication. However, despite their numerous advantages, UAVs face the challenge of limited onboard energy that dictates their operational time [4], [5], underscoring the need to optimize their operational efficiency. To this end, innovative methods are essential to harness the full potential of UAVs, while taking into account their energy constraints.

Given the finite flight duration of UAVs, it becomes of paramount importance to maximize data throughput and efficiency during their operational time. In this direction, full-duplex (FD) communication, with its ability to simultaneously transmit and receive data, emerges as a key solution in this context [6]. Unlike traditional half-duplex systems that alternate between transmission and reception, FD systems effectively double the spectral efficiency, making every time slot of the UAV's flight time count [6], [7]. This capability is particularly beneficial for UAVs, which can dynamically adjust their positions to establish LoS communication links, without the constraints of ground-based systems. To realize the potential of FD communications in UAVs, the two promising technologies that come to the forefront are reconfigurable intelligent surfaces (RISs) and FD relays (FDRs) [8], [9]. Specifically, an RIS is an advanced technology that can be implemented as either a programmable

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reflectarray or a programmable metasurface, both designed to manipulate electromagnetic (EM) waves for enhanced communication. Specifically, programmable reflectarrays offer dynamic backscattering and phase shifting of incident waveforms through omnidirectional antennas with controllable termination, while programmable metasurfaces extend these capabilities to include anomalous reflection angles and polarization manipulation [10]. This capability allows RIS to support FD communications by dynamically adjusting signal paths with minimal power requirements, significantly improving connectivity and signal quality [11], [12], [13]. On the other hand, FDRs enhance spectral efficiency by enabling simultaneous transmission and reception of signals over the same frequency channel, using distinct sets of antennas for each task [7], [14]. In addition, unlike RISs, the operation of FDRs is also based on the decode-and-forward (DF) protocol, which involves the decoding of the received message before forwarding, ensuring transmission of only accurately decoded messages. Therefore, as the integration of these technologies with UAVs continues to evolve, understanding their distinct advantages and challenges becomes crucial in shaping the future of UAV-assisted wireless networks.

A. Related Work

In recent years, the integration of UAVs with RIS and FDRs has gathered significant attention in the research community. Specifically, numerous studies have delved into the intricacies of UAV-mounted RIS and UAV-mounted FDRs, exploring various aspects ranging from performance optimization to energy efficiency, and underscoring their potential to reshape the dynamics of wireless communication.

1) *UAV-Mounted RIS*: As researchers explore ways to optimize wireless communications, the integration of UAVs with RISs emerges as a promising solution to maintain LoS links, especially in propagation environments where the wireless links can often be obstructed [15]. Specifically, Do et al. [16] showcased that UAV-mounted RIS can improve outage performance in dense urban scenarios, even with the dynamic mobility of UAVs. Additionally, [17] explored strategies for the optimal deployment of UAV-mounted RIS in URLLC systems, focusing on scenarios where user fairness is of paramount importance, while [18] proposed a novel system design that leverages ambient backscatter communication in UAV-mounted RIS networks. Interestingly, considering the different EM functionalities of RIS [11], Ptilakis et al. [19] provided a rigorous path loss model for the case where an UAV-mounted absorbing metasurface is utilized and validated the findings experimentally in an anechoic chamber. Transitioning to trajectory design, [20] emphasized on 3-D trajectory design for UAVs in urban environments, aiming to optimize the signal-to-noise ratio (SNR) for ground users, while [21] presented a trajectory optimization framework for UAV-mounted RIS focusing on maximizing the network's secure energy efficiency. Finally, [22] examined the joint optimization of the UAV trajectory design and the RIS design to facilitate the offloading of computational tasks in IoT networks. To this end, it is imperative to consider both

communication and trajectory design for realizing the full potential of UAV-mounted RIS in diverse wireless network scenarios.

2) *UAV-Mounted FDR*: While UAV-mounted RISs offer unique advantages in wireless communications, they are often challenged by significant path loss due to the double path loss phenomenon [12]. In contrast, UAV-mounted FDRs, equipped with integrated electronic components, such as amplifiers and decoders, not only have the capability to transmit and receive signals simultaneously but can also process the received signal, making them more robust to path loss than RISs. Therefore, UAV-mounted FDRs present a compelling solution, especially in dynamic environments demanding real-time data exchange and reduced latency [7], [9]. By taking into account the advantages of FDRs, [23] delved into optimizing the source and the UAV-mounted FDR transmit power along with its trajectory to enhance the system's outage probability. Furthermore, the potential of UAV-mounted FDRs in high-frequency scenarios was highlighted by [24] and [25], with a focus on millimeter-wave channels. Moreover, considering the increasing importance of secure communications, [26] introduced a secrecy communication scheme using an UAV-mounted FDR, optimizing various parameters to ensure both energy efficiency and security. Finally, [27] and [28] proposed an optimization algorithm for the UAV trajectory, user scheduling, and FDR power, showcasing significant performance improvements in scenarios with multiple ground users. Therefore, these recent research advances underscore the versatility of UAV-mounted FDRs in addressing diverse communication challenges in modern wireless networks.

B. Motivation and Contribution

In light of the aforementioned works, both RIS and FDR have been extensively compared to determine their respective advantages. However, a critical oversight concerning comprehensive energy consumption models in the analysis of UAV-mounted systems remains prevalent in the existing literature. For instance, while nearly passive, an RIS can become considerably larger due to the numerous reflecting elements, adding weight and impacting the UAV's energy efficiency [29]. Conversely, an FDR, though lightweight, demands more energy for tasks like decoding, amplification, and self-interference (SI) mitigation [25], [30]. Additionally, the different path loss characteristics of these systems introduce uncertainty in the UAV energy consumption for traversing, as the UAV may need to navigate to various locations to optimize path loss, further complicating the UAV energy consumption. To this end, neglecting detailed energy consumption models in trajectory optimization may lead to incomplete or imprecise assessments of the operational capabilities and limitations of UAV-mounted RIS and FDR systems. Building on this, few studies have focused on the performance of UAV-mounted systems, while considering their energy consumption profiles. For instance, [29] and [31] explored UAV-mounted RIS-based communications, emphasizing the RIS weight in UAV energy consumption and identifying an optimal number of reflecting elements, with the latter adjusting this number

with the addition of a solar panel. Finally, even though [32] compared UAV-mounted RIS with their relay counterparts, it overlooked the energy consumption characteristics and trajectory planning, thus potentially leading to incomplete conclusions. Therefore, to the best of the authors' knowledge, no existing work provides a comprehensive comparison of UAV-mounted RIS and UAV-mounted FDRs, especially in the context of optimal trajectory design, while considering their distinct energy consumption profiles.

In this article, a comprehensive analysis of both UAV-mounted RIS and UAV-mounted FDR employing the DF protocol is presented. In more detail, our contribution is the following.

- 1) We devise appropriate energy consumption models for both UAV-mounted RIS and UAV-mounted FDR that accurately capture the intricate relationship between key factors, such as weight, flight duration, and the operational needs of RISs and FDRs in terms of energy.
- 2) Recognizing the intricacies of UAV-mounted RIS and FDR setups, we formulate a joint time division multiple access (TDMA) user scheduling and UAV trajectory optimization problem that accounts for the power dynamics associated with both technologies. Given the nonconvex nature of this optimization problem, we employ a combination of alternate optimization and successive convex optimization techniques, ensuring an efficient approach to obtaining an approximate optimal solution.
- 3) Through simulation results, we demonstrate how our proposed methods significantly enhance the network minimum rate and user fairness. More specifically, our results show that for UAV-mounted RIS, increasing the number of reflecting elements does not necessarily translate into improved performance, largely due to the added weight of a larger RIS that limits operational flight time. In a notable shift from existing assumptions, the UAV-mounted FDR consistently outperforms the nearly passive RIS, which underscores the key role of UAV motors and the associated weight in overall UAV energy consumption. Additionally, the results highlight the crucial role of the UAV's battery capacity in trajectory optimization, directly influencing the optimal trajectory and thereby necessitating UAV movement only when it is essential for minimizing energy consumption during traversal. To this end, our work emphasizes the importance of energy-aware design in UAV-assisted communication networks, focusing on balancing energy consumption with communication efficiency.

C. Structure

The remaining of this article is organized as follows. The system model is described in Section II. Furthermore, the examined optimization problem and its solution is presented in Section III, while our simulation results are presented in Section IV. Finally, Section V concludes this article.

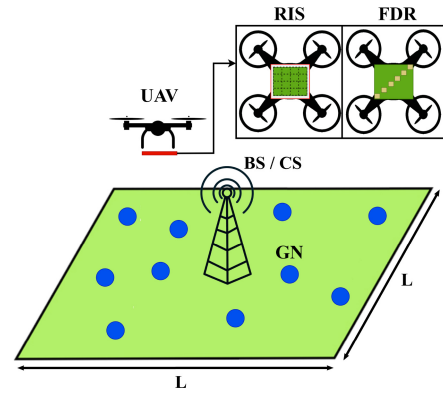


Fig. 1. UAV-assisted network topology.

II. SYSTEM MODEL

A. System Overview

We examine a network of K ground nodes (GNs) that are randomly distributed over a rectangular region with sides equal to L , and a base station (BS), which also operates as an UAV charging station (CS). However, given the challenging propagation conditions due to excessive distances, physical obstructions like buildings, and the GNs' limited transmission power, it is assumed that direct communication links between each GN and the BS are not available. To address this, we employ a rotary-wing UAV equipped with either an RIS or an FDR, to act as an intermediate assisting node between the GNs and the BS. Specifically, the UAV takes off from the BS and establishes LoS communication between the GNs and the BS, while flying along a designated trajectory. Afterward, the UAV returns to the BS for recharging purposes, leveraging the BS's dual functionality as a CS [33]. It should be highlighted that the examined network employs TDMA, a channel access method that allocates distinct time slots to multiple users within the same frequency band. This approach allows multiple GNs to share the same communication channel without interference, ensuring efficient service to different GNs within the UAV's flight duration. Finally, as illustrated in Fig. 1, it is crucial to ensure that the communication equipment is appropriately attached to the UAV frame to avoid disrupting the airflow around the motors and thus, compromising its aerodynamics and stability [31].

Considering a 3-D Cartesian coordinate system, we assume that the rectangular region's center coincides with the origin of the coordinate system, the BS location is equal to $\mathbf{l}_{\text{BS}} = [0, 0, H_{\text{BS}}]$, where H_{BS} represents the BS height, and the K GNs are located at $\mathbf{l}_{\mathbf{k}} = [x_{\mathbf{k}}, y_{\mathbf{k}}, 0]$, where $\mathbf{k} \in \{1, \dots, K\}$, respectively. Additionally, we assume that the UAV flies at a fixed altitude H_u , which is selected appropriately to ensure that the UAV navigates clear of any environmental obstacles. Furthermore, considering that the trajectory duration equals to T , the UAV location at time t can be written as $\mathbf{q}(t) = [x_q(t), y_q(t), H_u]$, where $0 \leq t \leq T$ and $(x_q(t), y_q(t))$ denote the x - y UAV coordinate at time t . However, for tractability reasons, the flight duration T is divided into N equal time slots, i.e., $T = N\delta_t$, where δ_t is the duration of each time slot. Hence, the UAV trajectory $\mathbf{q}(t)$ during T can be efficiently

approximated by an N -length sequence $\mathbf{q}_{[n]} = [x_{q[n]}, y_{q[n]}, H_u]$, $n \in \mathcal{N}$, $\mathcal{N} = \{1, \dots, N\}$, where $(x_{q[n]}, y_{q[n]})$ denote the $x - y$ UAV coordinate at n th time slot. Moreover, to derive the total number of time slots N associated with the UAV trajectory, it is essential to consider both the battery capacity of the available UAV battery and its overall power consumption. Specifically, given an UAV with a battery capacity B_c and an average power consumption per time slot of \bar{P}_d , the flight duration in time slots can be formulated as

$$N = \left\lfloor \frac{B_c}{\bar{P}_d} \right\rfloor \quad (1)$$

where $\lfloor \cdot \rfloor$ is the floor function and $d \in \{\text{RIS}, \text{FD}\}$ describes the communication equipment mounted on the UAV (i.e., RIS or FDR).

B. System's Achievable Rate

In order to deduce which is the most appropriate communication technology between RISs or FDRs to be mounted on an UAV, a thorough evaluation of the network performance is imperative. Therefore, below, we express the achievable rate of a network when the GN-BS communication is facilitated by either an UAV-mounted RIS or an UAV-mounted FDR.

1) *UAV-Mounted RIS*: Over the last years, RISs have emerged as efficient tools for manipulating EM waves with minimal energy consumption. Therefore, the integration of RISs on UAVs can offer a dynamic approach to wireless networks, as an UAV can optimally position an RIS to steer incoming EM waves directly to the BS, ensuring flexible 3-D network coverage. Hence, considering a reflectarray-based RIS that performs perfect beam-steering [12], the achievable rate of the k th GN in an UAV-mounted RIS-assisted TDMA network during the n th time slot is expressed as

$$R_{\text{RIS},k[n]} = Ba_{k[n]} \log_2 \left(1 + \ell_{\text{RIS}[n]} \gamma_{t[n]} GM^2 \right) \quad (2)$$

where B is the system's bandwidth and $a_{k[n]}$ is a binary variable that represents the time slot allocation in the TDMA network. Specifically, when $a_{k[n]} = 1$, it signifies that communication is established between the k th GN and the BS at the n th time slot. Moreover, $\ell_{\text{RIS}[n]}$ is the path loss that corresponds to the GN-RIS and RIS-BS links, respectively, which can be modeled through the double path loss model as

$$\ell_{\text{RIS}[n]} = \ell_{1[n]} \ell_{2[n]} = \frac{C_0 d_0^{n_p}}{(d_{1[n]})^{n_p}} \times \frac{C_0 d_0^{n_p}}{(d_{2[n]})^{n_p}} \quad (3)$$

where n_p is the path-loss exponent, $C_0 = (\lambda/4\pi)^2$ is the path loss of GN-UAV and UAV-BS links at the reference distance d_0 with λ denoting the wavelength, while $d_{1[n]}$ and $d_{2[n]}$ express the distances of the GN-UAV and the UAV-BS links at the n th time slot, respectively, and are equal to

$$d_{1[n]} = \|\mathbf{q}_{[n]} - \mathbf{l}_{k[n]}\| \quad (4)$$

and

$$d_{2[n]} = \|\mathbf{l}_{\text{BS}[n]} - \mathbf{q}_{[n]}\| \quad (5)$$

with $\|\cdot\|$ being the Euclidean norm. Moreover, M denotes the number of the RIS reflecting elements, $\gamma_{t[n]} = (P_{t[n]}/\sigma^2)$ is

the transmit SNR at the n th time slot, with $P_{t[n]}$ referring to the GN transmit power at the n th time slot and σ^2 referring to the additive white Gaussian noise (AWGN) affecting the BS, and $G = G_t G_r$ is the product of the GN and BS antenna gains. Finally, considering the LoS nature of air-to-ground communication links, the path loss exponent n_p is equal to 2. Consequently, the system's achievable rate is equal to

$$R_{\text{RIS},k[n]} = Ba_{k[n]} \log_2 \left(1 + \frac{\gamma_{t[n]} GC_0^2 d_0^4 M^2}{\underbrace{(d_{1[n]} d_{2[n]})^2}_{\gamma_{r,k[n]}^{\text{RIS}}} \right) \quad (6)$$

where $\gamma_{r,k[n]}^{\text{RIS}}$ is the SNR at the receiver side for the UAV-mounted RIS case when the k th GN is served. It should be mentioned that, in this work, we assume that all K GNs transmit with the same constant low power within the trajectory duration, thus $P_{t[n]} = P_t$ and $\gamma_{t[n]} = \gamma_t$.

2) *UAV-Mounted FDR*: An alternative solution that has been proposed for air-to-ground networking with improved spectral efficiency is to mount an FDR upon the UAV, referred to as UAV-mounted FDR [27]. Specifically, an UAV-mounted FDR with $A_n = A_r + A_t$ antennas can provide improved spectral efficiency as it is able to utilize simultaneously A_r antennas for reception and A_t antennas for transmission within one time slot, in contrast to conventional half-duplex relays, which utilize all of their antennas for distinct reception or transmission. However, it is imperative to note that in contrast to RISs, FDRs are inherently susceptible to SI, indicating the importance of advanced SI suppression techniques to optimize their operation. Nevertheless, the process of both analog and digital SI mitigation strategies has positioned FD relays for greater prominence in future network architectures [27]. To this end, assuming that the UAV-mounted FDR employs the DF protocol and that A_r antennas perform maximum ratio combining (MRC) and A_t antennas perform maximum ratio transmission (MRT) [34], the achievable rate of the k th GN within the n th time slot can be expressed as

$$R_{\text{FD},k[n]} = \min(R_{\text{FD},1[n]}, R_{\text{FD},2[n]}) \quad (7)$$

where $R_{\text{FD},1[n]}$ denotes the achievable rate from the k th GN to the UAV-mounted FDR at the n th time slot and $R_{\text{FD},2[n]}$ denotes the achievable rate from the UAV-mounted FDR to the BS at the n th time slot, and can be described as

$$R_{\text{FD},1[n]} = Ba_{k[n]} \log_2 \left(1 + \frac{P_t \ell_{1[n]} G_t A_r}{A_t G_r P_{u[n]} \omega + \sigma_1^2} \right) \quad (8)$$

and

$$R_{\text{FD},2[n]} = Ba_{k[n]} \log_2 \left(1 + \frac{A_t G_r P_{u[n]} \ell_{2[n]}}{\sigma_2^2} \right) \quad (9)$$

where $P_{u[n]}$ is the FDR transmit power at the n th time slot, $\sigma_1^2 = \sigma_2^2 = \sigma^2$ denote the variance of the AWGN affecting the FDR and the BS, respectively, and $\omega \in [0, 1]$ is the SI cancellation (SIC) coefficient. Finally, recalling the favorable

characteristics of air-to-ground communication links, i.e., $n_p = 2$, then $R_{\text{FD},1[n]}$ and $R_{\text{FD},2[n]}$ can be rewritten as

$$R_{\text{FD},1[n]} = Ba_{k[n]} \log_2 \left(1 + \frac{P_t C_0 d_0^2 G_t A_r}{\underbrace{d_{1[n]}^2 (A_t G_r P_{u[n]} \omega + \sigma^2)}_{\gamma_{1[n]}}} \right) \quad (10)$$

and

$$R_{\text{FD},2[n]} = Ba_{k[n]} \log_2 \left(1 + \frac{A_t G_r P_{u[n]} C_0 d_0^2}{\underbrace{d_{2[n]}^2 \sigma^2}_{\gamma_{2[n]}}} \right). \quad (11)$$

In addition, the SNR at the receiver side for the UAV-mounted FDR case when the k th GN is served is equal to

$$\gamma_{r,k[n]}^{\text{FD}} = \min(\gamma_{1[n]}, \gamma_{2[n]}). \quad (12)$$

It should be mentioned that similarly with the UAV-mounted RIS case, we assume that the GNs transmission power $P_{t[n]}$ is constant within the UAV flight, i.e., $P_{t[n]} = P_t$.

Remark 1: By setting $\gamma_{1[n]} = \gamma_{2[n]}$ we can derive the optimal FDR transmission power that maximizes the achievable rate of the k th GN at the n th time slot, which is given as

$$P_{u[n]}^* = \frac{-d_{1[n]} \sigma^2 + \sigma \sqrt{d_{1[n]}^2 \sigma^2 + 4\omega P_t d_{2[n]}^2 G_t A_r}}{2A_t G_r \omega d_{1[n]}}. \quad (13)$$

C. UAV Power Consumption

Given the inherent battery constraints of UAVs that result in finite flight duration, it becomes crucial to understand their power dynamics, particularly when integrating various communication technologies. Specifically, the UAV power consumption with varied communication equipment can be described as

$$P_{d[n]} = P_{\text{th},d[n]} + P_{c,d} + P_{\text{tr}} \quad (14)$$

where $P_{\text{th},d[n]}$ refers to UAV thrusting and encompasses the power demands for transitioning, countering wind drag, and related activities. Furthermore, $P_{c,d}$ denotes the power required by the communication equipment (e.g., RIS or FDR), while P_{tr} is a minimal constant power associated with the UAV's navigational communication (typically less than 1 W), and can be considered negligible [29]. To elaborate further on the required power for the consumption model, the required power for the reflectarray-based RIS operation $P_{c,\text{RIS}}$ can be described as

$$P_{c,\text{RIS}} = M P_e + P_{\text{ct}} \quad (15)$$

where P_e represents the power consumption of each reflecting element and P_{ct} refers to the energy required by the RIS controller to periodically adjust the RIS phase shift profile within every time slot. Furthermore, the power consumption for the FDR operation $P_{c,\text{FD}}$ is given as

$$P_{c,\text{FD}} = P_{u^*[n]}(1 + \alpha) + A_n P_R^C \quad (16)$$

where P_u is the FDR transmission power, α is the inverse of the power amplifier drain efficiency and P_R^C denotes the power consumption of an A_n -antenna transceiver [35]. This transceiver consumption encompasses the mixer power, the power of phase shifters for each antenna during transmission and reception, the power of each low-noise amplifier per antenna, the frequency synthesizer power, and the encoder power consumption.

Considering the inherent dynamics of UAVs, the thrusting power $P_{\text{th},d}$ plays a pivotal role in the total power consumption. Notably, $P_{\text{th},d}$ varies within each time slot, being heavily influenced by the UAV speed, its weight, aerodynamic design, and other onboard components, such as the battery weight. Thus, regarding the consumption model presented in [29], $P_{\text{th},d[n]}$ can be reliably characterized as

$$P_{\text{th},d[n]} = C_1 W_{d[n]}^2 + C_2 W_{d[n]} + C_3 \quad (17)$$

where C_1 , C_2 , and C_3 are motor-dependent parameters, while $W_{d[n]}$ encompasses all weight components impacting thrusting power, which can be expressed as

$$W_{d[n]} = U_w + D_w + R_{w,d} + S_{w,d[n]}. \quad (18)$$

In more detail, U_w expresses the weight of the UAV frame and its battery, while D_w describes the wind drag given as

$$D_w = \frac{\rho_a v_a^2 C_d A_{\text{UAV}}}{2g} \quad (19)$$

where ρ_a is the air density, g is the gravity acceleration, v_a is the average wind velocity, C_d is the drag shape coefficient given experimentally, and A_{UAV} is UAV frame area. Moreover, $R_{w,d}$ is the communication equipment weight, where in the RIS case is given by $R_{w,\text{RIS}} = M E_w$, while for an FDR with A_n antennas is equal to $R_{w,\text{DF}} = A_n A_w$, where E_w is the weight of one reflecting element and A_w is the weight of each FDR antenna, respectively. Finally, $S_{w,d[n]}$ is the extra weight added to the motors due to any change in the speed of the UAV in each time slot given by

$$S_{w,d[n]} = (T_{\text{max}} - U_w - D_w - R_{w,d}) \frac{v_{[n]}}{v_{\text{max}}} \quad (20)$$

with T_{max} being the maximum achievable thrust, $v_{[n]} = [(\|\mathbf{q}_{[n]} - \mathbf{q}_{[n-1]}\|)/\delta_t]$ reflecting the average UAV speed within the n th time slot, and v_{max} expressing the maximum achievable UAV speed. It should be mentioned that the choice of UAV motors is directly influenced by the weight they are required to lift. As such, an UAV-mounted RIS, which is generally heavier, would demand different motors than an UAV-mounted FDR, to stay in the air for the same amount of time slots as the UAV-mounted FDR. Finally, considering (1) and the available B_c , by setting $v_{[n]} = 0$ or $v_{[n]} = v_{\text{max}}$ in (20), we can obtain the maximum and the minimum flight duration in terms of time slots, i.e., N_{max} and N_{min} .

III. ENERGY-AWARE TRAJECTORY DESIGN

In this section, we formulate and solve an optimization problem to derive an UAV trajectory that maximizes the minimum data rate across K GNs, ensuring GN fairness across the network. Unlike existing works, our approach

underscores the importance of energy awareness, especially given the inherent battery constraints of UAVs. Specifically, our optimization problem intrinsically incorporates the UAV's power consumption, which is influenced by the mounted communication device, as well as the UAV velocity. Considering these energy dynamics, the formulated optimization problem not only ensures the practical relevance of our findings but also provides design insights into the characteristics of the employed RIS and FDR that optimize network performance. Moreover, the optimization guarantees that the power consumed by the UAV during its trajectory does not surpass its available battery energy, ensuring the UAV's safe return to the BS and highlighting the significance of energy-aware trajectory design. To this end, we will examine the network efficiency in terms of achievable rate and fairness for both RIS and FDR.

A. Problem Formulation

To efficiently maximize the minimum data rate of the network, we aim to jointly optimize the UAV trajectory and TDMA user scheduling, taking into account mobility, user scheduling, and UAV power consumption constraints. Given these considerations, by leveraging the integer variable \mathbf{A} that represents the TDMA scheduling, and the continuous variable \mathbf{Q} that describes the UAV trajectory, the optimization problem for both UAV-mounted RIS and UAV-mounted FDR cases can be formulated as

$$\begin{aligned}
 & \max_{\mathbf{A}, \mathbf{Q}} \min_k \left\{ \sum_{n=1}^N R_{d,k[n]} \right\} \\
 \text{s.t. } & C_1 : \mathbf{q}_{[1]} = \mathbf{q}_{[N]} \\
 & C_2 : v_{[n]} \leq v_{\max} \quad \forall n \in \mathcal{N} \\
 & C_3 : \sum_{k=1}^K a_{k[n]} \leq 1 \quad \forall n \in \mathcal{N} \\
 & C_4 : B_c - \delta_t \sum_{n=1}^N P_{d[n]} \geq 0 \\
 & C_5 : a_{k[n]} \in \{0, 1\} \quad \forall n \in \mathcal{N} \\
 & C_6 : q_{\min} \leq \mathbf{q}_{[n]} \leq q_{\max} \quad \forall n \in \mathcal{N} \\
 & C_7 : P_{u[n]} \leq P_{\max} \quad \forall n \in \mathcal{N} \quad (\text{P1})
 \end{aligned}$$

where $R_{d,k[n]}$ is the GN data rate which is given by

$$R_{d,k[n]} = \begin{cases} 0, & \gamma_{r,k[n]}^d < \gamma_{\text{thr}} \\ Ba_{k[n]} \log_2 \left(1 + \gamma_{r,k[n]}^{\text{RIS}} \right), & \gamma_{r,k[n]}^d > \gamma_{\text{thr}}, d = \text{RIS} \\ Ba_{k[n]} \log_2 \left(1 + \gamma_{r,k[n]}^{\text{FDR}} \right), & \gamma_{r,k[n]}^d > \gamma_{\text{thr}}, d = \text{FDR} \end{cases} \quad (21)$$

where γ_{thr} is an SNR threshold. In more detail, C_1 forces the UAV trajectory to begin and end at the same point. In addition, C_2 indicates that the UAV speed $v_{[n]}$ cannot exceed the maximum UAV velocity v_{\max} , while C_3 defines that only one GN-BS pair can be served by the UAV-mounted RIS or the UAV-mounted FDR within a certain time slot. Moreover, C_4 indicates that the UAV's power consumption during its

trajectory must not exceed its battery's available energy, while C_5 and C_6 set the lower and upper bounds for the optimization variables \mathbf{a} and \mathbf{q} , with C_6 ensuring the UAV remains within the predefined rectangular field. Finally, C_7 describes that the UAV's transmission power should be less than P_{\max} , denoting the peak power limit of the UAV, where for the UAV-mounted RIS case, $P_{u[n]} = 0$ as the RIS does not consume any transmission power.

B. Problem Solution

As it can be seen, problem (P1) is intractable since it contains both continuous and integer variables while its objective function is nonconvex. To this end, given that current optimization methods struggle with problems containing nonlinear constraints paired with integer variables, a separation of the integer variable \mathbf{A} and the continuous variable \mathbf{Q} becomes essential. To address this, the alternate optimization technique is employed, which relies on successively optimizing each optimization variable block until convergence [27]. Therefore, for a fixed trajectory \mathbf{Q} we have

$$\begin{aligned}
 & \max_{\mathbf{A}} \min_k \left\{ \sum_{n=1}^N R_{d,k[n]} \right\} \\
 \text{s.t. } & C_1 : \sum_{k=1}^K a_{k[n]} \leq 1 \quad \forall n \in \mathcal{N} \\
 & C_2 : a_{k[n]} \in \{0, 1\} \quad \forall n \in \mathcal{N}. \quad (\text{PA.1})
 \end{aligned}$$

As it can be seen, problem (PA.1) is an integer programming problem, however, it is not in canonical form, since the objective function is a nonlinear function. Thus, by utilizing the auxiliary variable r_{\min} , problem (PA.1) is equivalently written as

$$\begin{aligned}
 & \max_{\mathbf{A}, r_{\min}} r_{\min} \\
 \text{s.t. } & C_1 : \sum_{k=1}^K a_{k[n]} \leq 1 \quad \forall n \in \mathcal{N} \\
 & C_2 : a_{k[n]} \in \{0, 1\} \quad \forall n \in \mathcal{N} \\
 & C_3 : \sum_{n=1}^N a_{k[n]} R_{d,k[n]} \geq r_{\min} \quad \forall k \in \mathcal{K} \quad (\text{PA.2})
 \end{aligned}$$

which is a mixed-integer linear programming problem (MILP), since for given trajectory \mathbf{Q} , $R_{d,k[n]}$ is constant for either the FDR or the RIS case. As a consequence, (PA.2) can be optimally solved using off-the-self optimization tools, such as the branch and bound method.

1) *Optimization of \mathbf{Q}* : Given the TDMA schedule \mathbf{A} , problem (P1) can be written as

$$\begin{aligned}
 & \max_{\mathbf{Q}} \min_k \left\{ \sum_{n=1}^N a_{k[n]} R_{d,k[n]} \right\} \\
 \text{s.t. } & C_1 : \mathbf{q}_{[1]} = \mathbf{q}_{[N]} \\
 & C_2 : v_{[n]} \leq v_{\max} \quad \forall n \in \mathcal{N} \\
 & C_3 : B_c - \delta_t \sum_{n=1}^N P_{d[n]} \geq 0
 \end{aligned}$$

$$\begin{aligned} C_4 : q_{\min} &\leq \mathbf{q}[n] \leq q_{\max} \quad \forall n \in \mathcal{N} \\ C_5 : P_{u[n]} &\leq P_{\max} \quad \forall n \in \mathcal{N} \end{aligned} \quad (\text{PQ.1})$$

which is a nonconvex problem due to the nonconcave and dual branch objective function $R_{d,k[n]}$. Furthermore, in (20), $P_{d[n]}$ is influenced by the UAV's speed $v[n]$, which is derived from the differences in consecutive positions $x_{q[n]}$ and $y_{q[n]}$, thus, given that these positions are constants for each time slot, the relationship of $P_{d[n]}$ with x_q and y_q is affine, as it comprises linear differences and constant terms. Thus, $P_{d[n]}$ is by definition convex which makes constraint C_3 convex as well. In addition, by introducing the auxiliary variable r_{\min} , problem (PQ.1) is equivalently transformed as follows:

$$\begin{aligned} &\max_{x_q, y_q, r_{\min}} r_{\min} \\ \text{s.t. } &(\text{PQ.1}) : C_1, C_2, C_3, C_4, C_5 \\ &C_6 : \sum_{\substack{n=1 \\ a_{k[n]}=1}}^N R_{d,k[n]} \geq r_{\min} \quad \forall k \in \mathcal{K}. \end{aligned} \quad (\text{PQ.2})$$

Again, problem (PQ.2) is still nonconvex due to C_6 . To tackle this, we can convert it from a dual branch function into a single function by introducing an appropriate constraint that assures that the UAV always serves a GN for which the received SNR at the BS-side is above γ_{thr} . Additionally, $\forall n \in \mathcal{N}$ and $\forall k \in \mathcal{K}$ for which $a_{k[n]} = 1$, we can introduce the auxiliary variables $r_{k[n]}$, thus the problem (PQ.2) can be rewritten as

$$\begin{aligned} &\max_{x_q, y_q, r_{\min}, r_{k[n]}} r_{\min} \\ \text{s.t. } &(\text{PQ.1}) : C_1, C_2, C_3, C_4, C_5 \\ &C_6 : \sum_{\substack{n=1 \\ a_{k[n]}=1}}^N r_{k[n]} \geq r_{\min} \quad \forall k \in \mathcal{K} \\ &C_7 : \gamma_{r,k[n]}^d \geq \gamma_{\text{thr}} \quad \forall n \in \mathcal{N} \quad \forall k \in \mathcal{K} \text{ that } a_{k[n]} = 1 \\ &C_8 : R_{d,k[n]} \geq r_{k[n]} \quad \forall n \in \mathcal{N} \quad \forall k \in \mathcal{K} \text{ that } a_{k[n]} = 1. \end{aligned} \quad (\text{PQ.3})$$

Due to the distinct achievable rates of the UAV-mounted RIS and the UAV-mounted FDR, C_7 and C_8 have to be dealt differently for each case. To this end, the distinct approaches for the two cases are presented below.

- 1) *UAV-Mounted RIS*: Utilizing (6) and defining $A_R = \gamma_l G C_0^2 d_0^4 M^2$, we adopt the approximation $\log_2(1+z) \approx \log_2(z)$. This choice is motivated by the dominant high SNR conditions inherent in our system, particularly under LoS scenarios. In fact, given the UAV's strategic positioning relative to the GNs it serves, z is typically large, making the approximation increasingly pertinent. Thus, C_8 can be expressed as

$$C_8 : \log_2(d_{1[n]}^2) + \log_2\left(\frac{d_{2[n]}^2}{A_R}\right) \leq -r_{k[n]}. \quad (22)$$

Furthermore, by introducing the auxiliary variables $s_{k,n}$ and $t_{k[n]}$, such that $\log_2(d_{1[n]}^2) \leq s_{k,n}$ and $\log_2(d_{2[n]}^2) \leq t_{k[n]}$, C_6 and C_8 are rewritten as

$$C_6 : \sum_{n=1}^N (s_{k[n]} + t_{k[n]}) \leq -r_{\min}$$

$$C_8 : s_{k[n]} + t_{k[n]} \leq -r_{k[n]} \quad (23)$$

while the following constraints occur as well:

$$\begin{aligned} C_{8.A} : &(x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2 - 2^{s_{k,n}} \leq 0 \\ C_{8.B} : &\frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{\text{BS}})^2}{A_R} \\ &- 2^{t_{k[n]}} \leq 0. \end{aligned} \quad (24)$$

We note that C_7 can be handled in the same way, by introducing the auxiliary variables $\hat{s}_{k[n]}$ and $\hat{t}_{k[n]}$. Then, the convex form of C_7 is equivalently given as follows:

$$\begin{aligned} C_7 : &\hat{s}_{k[n]} + \hat{t}_{k[n]} \leq -\log(\gamma_{\text{thr}}) \\ C_{7.A} : &(x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2 - 2^{\hat{s}_{k[n]}} \leq 0 \\ C_{7.B} : &\frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{\text{BS}})^2}{A_R} \\ &- 2^{\hat{t}_{k[n]}} \leq 0. \end{aligned} \quad (25)$$

To address the nonconvexity introduced by the new constraints $C_{7.A}$, $C_{7.B}$, $C_{8.A}$, and $C_{8.B}$, the successive approximation method (SCA) is employed [27]. Thus, by substituting the nonconvex terms with their first-order Taylor approximation, we formulate the convex optimization problem for the trajectory design in the UAV-mounted RIS scenario as follows:

$$\begin{aligned} &\max_{x_q, y_q, r_{\min}, r_{k[n]}, s_{k,n}, t_{k[n]}} r_{\min} \\ \text{s.t. } &(\text{PQ.3}) : C_1, C_2, C_3, C_4, C_5, C_6, C_7, C_8 \\ &C_{7.A} : (x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2 \\ &\quad - 2^{\hat{s}_{k[n],0}} - (\hat{s}_{k[n]} - \hat{s}_{k[n],0})2^{\hat{s}_{k[n],0}} \leq 0 \\ &C_{7.B} : \frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{\text{BS}})^2}{A_R} \\ &\quad - 2^{\hat{t}_{k[n],0}} - (\hat{t}_{k[n]} - \hat{t}_{k[n],0})2^{\hat{t}_{k[n],0}} \leq 0 \\ &C_{8.A} : (x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2 \\ &\quad - 2^{s_{k[n],0}} - (s_{k,n} - s_{k[n],0})2^{s_{k[n],0}} \leq 0 \\ &C_{8.B} : \frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{\text{BS}})^2}{A_R} \\ &\quad - 2^{t_{k[n],0}} - (t_{k[n]} - t_{k[n],0})2^{t_{k[n],0}} \leq 0 \quad (\text{PQ.4-RIS}) \end{aligned}$$

where $s_{k[n],0}$, $t_{k[n],0}$, $\hat{s}_{k[n],0}$, and $\hat{t}_{k[n],0}$ are the arbitrary initial points for the Taylor approximation.

Remark 2: For the case in the UAV-mounted RIS scenario where the trajectory's initial point coincides with the BS location and the path loss exponents of the BS-RIS and RIS-GN channels are equal, the optimal trajectory is to hover at this point until the UAV's battery is depleted. This strategy maximizes the network's data rate by achieving the minimum overall path loss through minimal UAV-BS distance due to the double path loss phenomenon, and simultaneously minimizes energy consumption, capitalizing on the UAV's hovering state.

- 2) *UAV-Mounted FDR*: For the UAV-mounted FDR case, the C_7 can be equivalently written as

$$C_{7,A} : \frac{(x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2}{A_{FD,1[n]}} \leq \frac{1}{\gamma_{thr}}$$

$$C_{7,B} : \frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{BS})^2}{A_{FD,2[n]}}$$

$$\leq \frac{1}{\gamma_{thr}} \quad (26)$$

which is convex. Furthermore, by utilizing (7), (10), (11), and considering that the condition $\min\{x, y\} \geq t$ implies that both $x \geq t$ and $y \geq t$, thus, C_8 in **PQ.3** can be equivalently divided into two separate constraints

$$C_{8,A} : \log_2(A_{FD,1[n]} d_{1[n]}^{-2}) \geq r_{k[n]}$$

$$C_{8,B} : \log_2(A_{FD,2[n]} d_{2[n]}^{-2}) \geq r_{k[n]} \quad (27)$$

where $A_{FD,1[n]} = [(P_t C_0 d_0^2 G_t A_r) / (A_t G_r P_{u[n]} \omega + \sigma^2)]$ and $A_{FD,2[n]} = [(A_t G_r P_{u[n]} C_0 d_0^2) / \sigma^2]$. Finally, similarly to the UAV-mounted RIS case, we utilize the SCA method, thus the trajectory optimization problem for the UAV-mounted FDR case is given as

$$\begin{aligned} & \max_{x_q, y_q, r_{\min}, r_{k[n]}} \\ & \text{s.t. (PQ.3)} : C_1, C_2, C_3, C_4, C_5, C_6, C_7, C_8 \\ & C_{8,A} : \frac{(x_{q[n]} - x_k)^2 + (y_{q[n]} - y_k)^2 + H_u^2}{A_{FD,1[n]}} \\ & \quad - 2^{r_{k[n],0}} - (r_{k[n]} - r_{k[n],0}) 2^{r_{k[n],0}} \leq 0 \\ & C_{8,B} : \frac{(x_{q[n]} - x_b)^2 + (y_{q[n]} - y_b)^2 + (H_u - H_{BS})^2}{A_{FD,2[n]}} \\ & \quad - 2^{r_{k[n],0}} - (r_{k[n]} - r_{k[n],0}) 2^{r_{k[n],0}} \leq 0. \quad (\text{PQ.4-FDR}) \end{aligned}$$

As it can be observed, both problem (PQ.4-RIS) and problem (PQ.4-FDR) are now convex, allowing them to be addressed using standard optimization techniques like the interior-point method. The procedure for the joint TDMA-trajectory design, for both the UAV-mounted RIS and UAV-mounted FDR cases, is outlined in Algorithm 1. It is worth noting that the values for iter_1 and iter_2 are selected to ensure that the solutions from both the SCA and alternate optimization methods converge to a consistent solution [27], which is then presented as the final output of Algorithm 1.

IV. SIMULATION RESULTS

In this section, we present numerical results to assess the performance of the proposed UAV-assisted communication scenarios, whose power consumption and network parameters are set as detailed in Tables I and II, respectively. Specifically, we consider an uplink communication system assisted by 1) an UAV-mounted RIS or 2) an UAV-mounted FDR with ten GNs that transmit with power equal to $P_t = 0$ dBm, that are also randomly distributed over a rectangular area with sides equal to $L = 750$ m, unless otherwise stated. In addition, a single-antenna BS is located in the origin of the rectangular area which also serves as an UAV CS. It should

Algorithm 1 Trajectory Design for UAV-Mounted RIS or UAV-Mounted FDR

```

1: Initialize  $\text{iter}_1, \text{iter}_2, B_c, \delta_t, v_{\max}, U_w, D_w, R_{w,d}$ 
2: for  $N = N_{\min}, N_{\min} + 1, \dots, N_{\max}$  do
3:   Initialize  $A_{\text{init}}, Q_{\text{init}}$ 
4:   for  $i = 0, 1, 2, \dots, \text{iter}_1$  do
5:     For  $Q_{\text{init}}$ , solve (PA.2) and obtain  $A^i$ 
6:     for  $j = 0, 1, 2, \dots, \text{iter}_2$  do
7:       For  $A^i$ , solve (PQ.4-FDR) or (PQ.4-RIS)
       and obtain  $Q^j$ 
8:        $r_{k[n],0}^j \leftarrow r_{k[n],0}^j, s_{k[n],0}^j \leftarrow s_{k[n],0}^j, t_{k[n],0}^j \leftarrow t_{k[n],0}^j$ 
9:     end for
10:     $Q_{\text{init}} \leftarrow Q^{\text{iter}_2}$ 
11:  end for
12:   $Q^* \leftarrow Q^{\text{iter}_2}$ 
13:  For  $Q^*$ , solve (PA.2) and obtain  $A^*$ 
14: end for
15: Obtain the best  $Q^*$  and  $A^*$ 

```

TABLE I
POWER CONSUMPTION MODEL PARAMETERS

Parameter	Notation	Value
UAV weight	U_w	3.25 kg
Reflecting element weight	E_w	3.43×10^{-3} kg
Antenna weight	A_w	8×10^{-3} kg
Battery weight	B_w	1.35 kg
Battery capacity	B_c	45 Wh
Reflecting element consumption	P_n	$2 \mu\text{W}$
Controller consumption	P_c	50 mW
Inverse of pow. ampl. drain eff.	α	1.875
Transceiver consumption	P_R^C	1.5 W
Maximum achievable thrust	T_{\max}	17 kg
Maximum UAV speed	v_{\max}	62 km/h
Air density	ρ_a	1.225 kg/m^3
Air velocity	v_a	2.5 m/s (Light Air)
Drag shape coefficient	C_d	0.005
UAV frame	A_{UAV}	$0.5 \times 0.5 \text{ m}^2$
Reflecting element area	A_{re}	$\frac{\lambda}{10} \times \frac{\lambda}{10} \text{ m}^2$
Gravity acceleration	g	9.8 m/s^2
MN505-s KV320 T-MOTOR	C_1, C_2, C_3	4, 86, -21.2
AT4130 KV230 T-MOTOR	C_1, C_2, C_3	10.5, -46, 744

TABLE II
NETWORK PARAMETERS

Parameter	Notation	Value
UAV height	H_u	100 m
BS height	H_{BS}	15 m
Number of GNs	K	10
Max transmit FDR power	P_{\max}	0 dBm
time slot duration	δ_t	1 s
Reference distance	d_0	1 m
Bandwidth	B	1 MHz
Transmit power	P_t	0 dBm
Noise Power	σ^2	-144 dBm
Antenna gains	G_t, G_r	0 dB
Wavelength	λ	0.125 m
SIC coefficient	ω	-90 dB
Iterations	$\text{iter}_1, \text{iter}_2$	20, 20

be mentioned that, in alignment with practical scenarios, we assume that the UAV starts and concludes its trajectory at the same location, reflecting the common practice, where the UAV takes off and lands at the same place for recharging purposes. Moreover, it is assumed that the UAV-mounted RIS

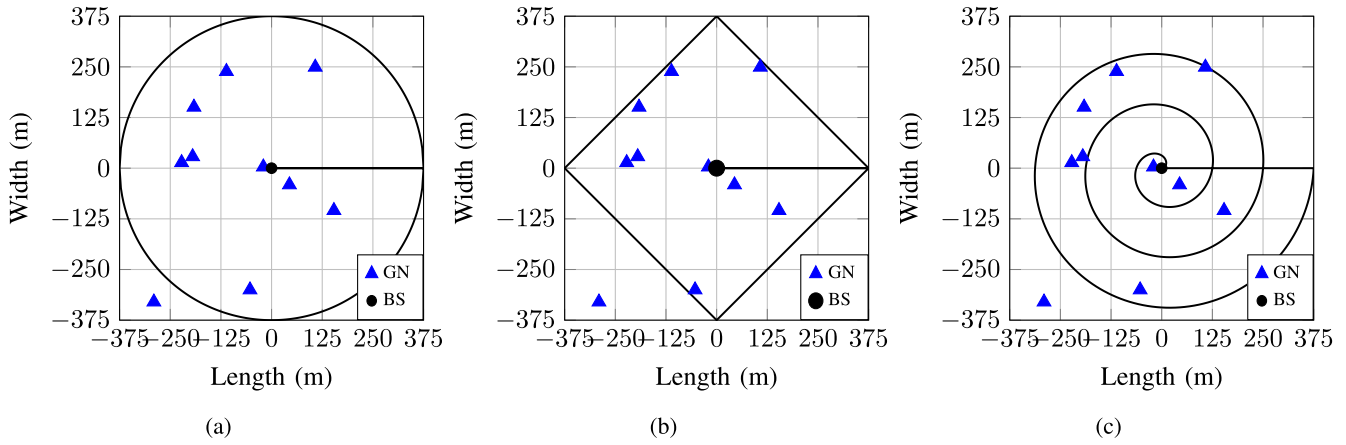


Fig. 2. Benchmark UAV trajectories. (a) Circle. (b) Rhombus. (c) Spiral.

is equipped with the MN505-s KV320 T-MOTOR motors due to its weight, while the lighter UAV-mounted FDR uses the AT4130 KV230 T-MOTOR motors. Moreover, the size of the UAV frame, combined with the size of each reflecting element as outlined in Table I, allows for a maximum of 1600 reflecting elements to be fitted on the UAV frame. In contrast, for the UAV-mounted FDR, the frame can accommodate a maximum of 12 antennas, arranged as an uniform linear array (ULA) with an interdistance of $(\lambda/2)$ along the frame's diagonal, for which we assume that $A_t = A_r$. In addition, we consider a benchmark TDMA scheduling scheme where each GN is allocated $N_{GN} = \lfloor N/K \rfloor$ time slots, to clearly show the efficiency of our algorithm. To be more precise, in the benchmark scheme, the UAV serves the nearest GN for N_{GN} time slots and then serves the next nearest unserved GN, continuing until every GN has been served before returning to its initial location. Additionally, the benchmark trajectories are determined through a detailed search for the most effective combination of time slots and trajectory sizes, all considered within the operational limits of the UAV's battery life. Finally, all of the results were calculated through Monte Carlo simulations with 1000 iterations.

In Fig. 2, three distinct benchmark UAV trajectories are illustrated, each serving as a feasible initial trajectory, denoted as \mathcal{Q}_{init} , for the implementation of Algorithm 1. These trajectories include 1) a straight line connecting the origin to the midpoint on the right side of the rectangular field, followed by a circle with radius $(L/2)$ centered at the axis origin; 2) a straight line connecting the origin to the midpoint on the right side of the rectangle, succeeded by a rhombus with sides measuring $(L\sqrt{2}/2)$; and 3) an Archimedean spiral described in polar coordinates by $r = (L/12\pi)\theta$, with $\theta \in [0, 2\pi)$, followed by a straight line leading back to the origin. In the circular and rhombus trajectories, the UAV initially follows the straight line, completes the circle or rhombus, and then retraces its path along the straight line back to the origin, while in the spiral trajectory the UAV navigates the spiral path before returning to the origin via the straight line. Notably, in all these trajectories, the UAV navigates counter-clockwise, with the starting and ending points, $\mathbf{q}_{[1]}$ and $\mathbf{q}_{[N]}$, aligning with the BS location. It should be highlighted that as shown

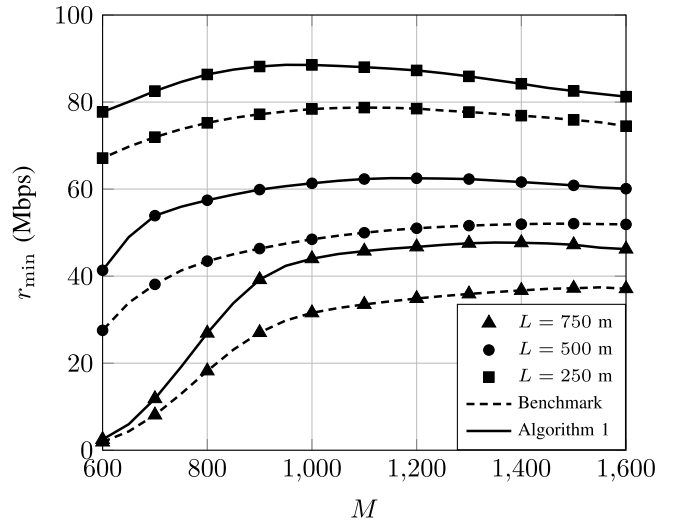


Fig. 3. Minimum rate versus the number of reflecting elements M for $\sigma^2 = -144$ dB.

in (1), the calculation of N based on B_c and P_d informs the minimum average speed required for the UAV to deplete its battery at the final point of the trajectory, thereby defining the feasible size of each trajectory within the allocated time slots. Specifically, the maximum number of time slots corresponds to the case where the UAV minimizes its power consumption (i.e., hovering), while reducing the number of time slots allows for larger trajectories. This indicates that an optimal number of time slots must be determined, as too many slots could restrict the UAV from performing large enough trajectories due to energy limitations, while fewer slots may limit service duration. Thus, the evaluation of different initial trajectories, each corresponding to a specific number of time slots is demanded, which can be done by initializing different values of N in step 1 of Algorithm 1 and selecting the value of N maximizing r_{min} .

In Fig. 3, we illustrate the relationship between the network's minimum rate r_{min} and the number of reflecting elements on the UAV-mounted RIS, with the noise power set at $\sigma^2 = -144$ dB, for $L = 750$, 500 , and 250 m, respectively. As it can be observed, r_{min} increases as L decreases, which

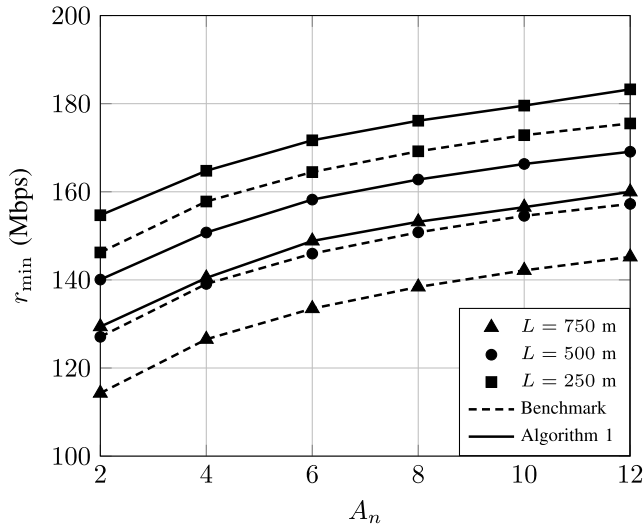


Fig. 4. Minimum rate versus UAV-mounted FDR antennas for $\sigma^2 = -144$ dB.

is a consequence of the reduced path loss for the GNs. As it can be observed, across all examined L cases, there exists an optimal number of reflecting elements which results from the improved channel gains and the increased energy consumption due to the weight of additional elements. Specifically, adding more reflecting elements increases the rate for each GN logarithmically, while the number of time slots decreases quadratically, in lines with (14) and (17) for the case where the UAV speed is equal to zero (i.e., hovering state). Moreover, Fig. 3 shows that for larger L values, a higher number of reflecting elements is optimal, suggesting a strategy to mitigate excess path loss with shorter flight durations. However, in smaller areas, a precise selection of reflecting elements is essential, as fewer elements can achieve enhanced coverage, thus negating the need for further increasing the reflecting elements and avoiding a compromise on the flight duration. Additionally, a key observation is the impact of the optimized user scheduling by Algorithm 1, which significantly reduces the required number of reflecting elements. For instance, under the benchmark scheduling for $L = 750$, 500, and 250 m, the optimal numbers of reflecting elements are 1550, 1500, and 1100, respectively, while with optimized user scheduling, these numbers reduce to 1350, 1150, and 950, respectively, emphasizing the advantages of network optimization in determining the optimal RIS size. Finally, in line with Remark 2, the optimal trajectory obtained from Algorithm 1 for the UAV-mounted RIS scenario, considering that $q_{[1]}$ coincides with the BS location, is the hovering trajectory, maximizing the minimum rate through minimized path loss and optimized energy use.

Fig. 4 shows the effect of the number of antennas on the UAV-mounted FDR on r_{\min} , for $\sigma^2 = -144$ dB and $L = 750$, 500, and 250 m, respectively. As it can be seen, decreasing the value of L and increasing the number of FDR antennas enhances r_{\min} , with 12 antennas emerging as the optimal number for network performance. Furthermore, similarly to the UAV-mounted RIS scenario, the application of Algorithm 1

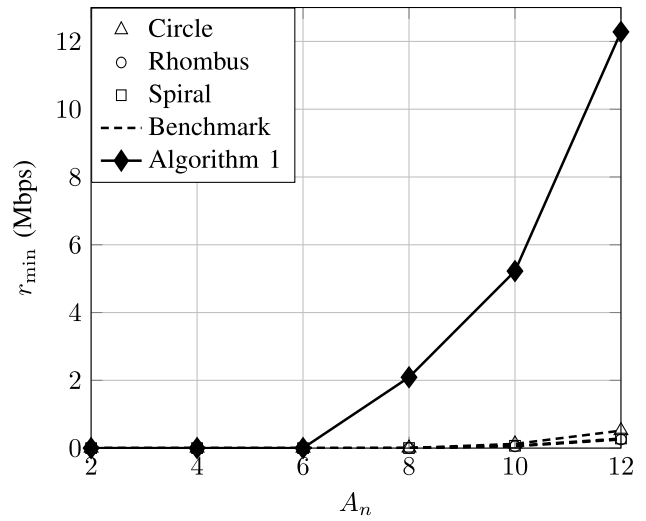


Fig. 5. Minimum rate versus UAV-mounted FDR antennas for $\sigma^2 = -114$ dB and $L = 750$ m.

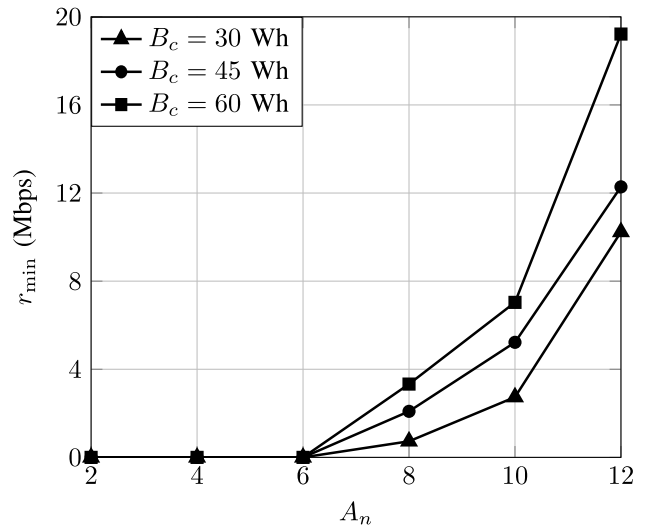


Fig. 6. Minimum rate versus UAV-mounted FDR antennas for $\sigma^2 = -114$ dB and $L = 750$ m for various battery capacities.

further enhances the minimum rate, demonstrating its value on the network performance improvement. Interestingly, under the network parameters in Table II, Algorithm 1 identifies the hovering trajectory as the optimal approach for all the examined cases, which is a notable deviation from the expected optimization of the UAV-mounted FDR's path loss at intermediate distances between a GN and the BS. Specifically, for the given network parameters, the received SNR for the GNs consistently stays above γ_{thr} across all L values, influencing the trajectory design, as it leads to the conclusion that maximizing the flight duration, thus serving the GNs from the initial UAV position, is more advantageous than moving the UAV to each GN's optimal point, which results in the loss of time slots. In more detail, during the UAV's traversal to these optimal points, there would be instances where the UAV is not optimally positioned to serve any GN, leading to inefficient use of energy and further loss of time slots. Finally, the results from Figs. 3 and 4 indicate that

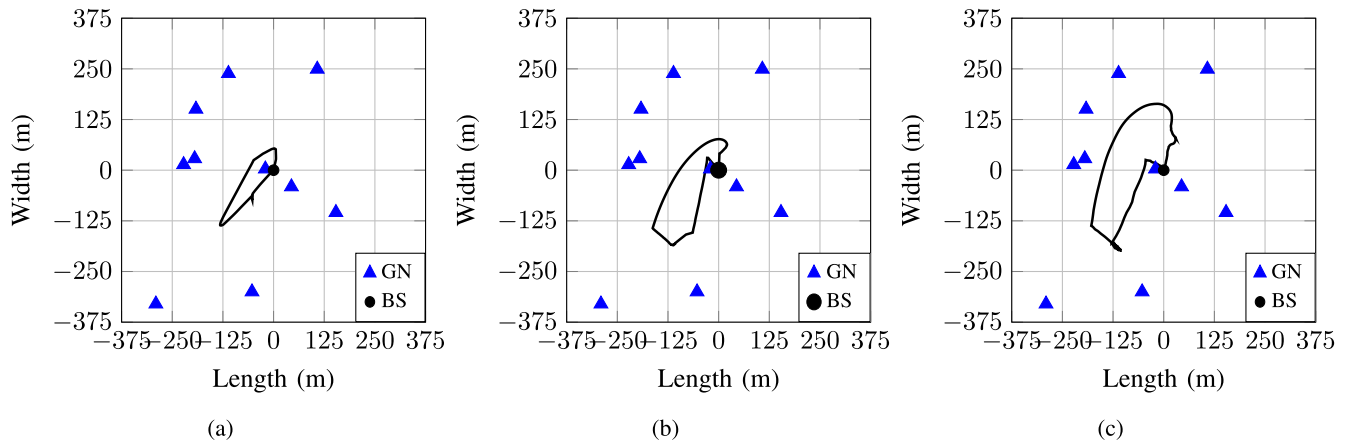


Fig. 7. Optimal UAV trajectories. (a) $B_c = 30$ Wh. (b) $B_c = 45$ Wh. (c) $B_c = 60$ Wh.

the UAV-mounted FDR outperforms the UAV-mounted RIS for all values of L , even with two antennas on the FDR. This superior performance of the FDR is attributed to the severe impact of double path loss in the RIS scenario and the FDR's lower energy consumption compared to the RIS, which incurs significant energy costs due to its weight. Additionally, the UAV-mounted FDR's performance is favored as no extra energy is consumed for transitioning, despite potential path loss optimization for each GN. To this end, the provided results underscore the practical implications of UAV system choices on network performance, particularly emphasizing the balance between energy consumption and effective communication, while also highlighting the significant effect of the UAV motors over the energy required for the RIS and FDR operation in the UAV energy consumption.

Fig. 5 illustrates the trajectory optimization for an UAV-mounted FDR, comparing the solution from Algorithm 1 with the benchmark trajectories for which the benchmark TDMA scheme is applied, in a scenario with an increased noise power of -114 dB for an area of L equal to 750 m. In this scenario, unlike in Fig. 4 where $\sigma^2 = -144$ dB and the UAV-mounted FDR remains stationary, the increased noise level results in areas where, if GNs are located within them, the received SNR falls below γ_{thr} , UAV movement is necessary to maintain effective communication. As it can be seen, for $A_n = 12$, the circular trajectory achieves a minimum rate of 0.51 Mb/s, the rhombus 0.25 Mb/s, and the spiral 0.28 Mb/s, while the trajectory optimized through Algorithm 1s leads to a significantly higher rate of 12.28 Mb/s. Moreover, for all examined trajectories, when the number of A_n is less than 6 , the network's minimum rate tends toward zero, due to the increased probability of GNs experiencing outages and the UAV's battery limitations, which are insufficient to enable the UAV to serve all GNs effectively. Therefore, Fig. 5 emphasizes the critical interplay between the number of antennas, UAV battery capacity, and trajectory optimization in ensuring robust network performance, especially in scenarios with challenging communication conditions, such as increased noise or γ_{thr} thresholds. Finally, it should be noted that for the UAV-mounted RIS case, if $\sigma^2 = -114$ dB then $r_{\text{min}} = 0$ across all the feasible M values, proving again the superiority of

UAV-mounted FDR over UAV-mounted RIS in establishing communication link between the BS and the GNs.

Finally, Fig. 6 depicts how r_{min} is affected by the number of antennas A_n of an UAV-mounted FDR across various battery capacities, B_c , showcasing how an increase in B_c leads to an improvement in the network's minimum rate. Specifically, this enhancement occurs due to the UAV's ability to allocate more time slots for serving each GN, which not only allows for more extensive service coverage but also enables the UAV to fly to more optimal locations for serving each GN, as the increased number of time slots extends the operational time before the battery depletes. Furthermore, Fig. 6 also indicates that larger battery capacities permit the UAV to execute broader trajectories, optimizing its positioning across the field to serve the GNs more effectively, while smaller battery capacities limit the trajectory size. Complementing this, Fig. 7 illustrates the optimal trajectory for a specific GN setup, which depicts the expansion in the size of the UAV's trajectory as B_c increases. This expansion reflects the variation in the optimal number of time slots needed for different B_c , illustrating the direct relation between battery capacity and the effectiveness of the UAV's flight path in enhancing network performance. Additionally, a notable aspect of these trajectories in Fig. 7, is the formation of a distinct spike in the bottom-left region of the trajectory for all analyzed battery capacities, which is a consequence of the strategic positioning needed to address the unfavorable location of the bottom-left GNs within the rectangular area. This contrasts with the right-hand side of the rectangular area, where the GNs are fewer in number, leading to a different trajectory pattern that does not necessitate such pronounced adjustments. To this end, Figs. 6 and 7 underscore the effect of the battery capacity on trajectory optimization, while emphasizing their significance in ensuring robust network performance, particularly in scenarios with demanding communication conditions.

V. CONCLUSION

In this work, a thorough comparison between UAV-mounted RIS and UAV-mounted FDRs was performed, highlighting their distinct energy consumption patterns and underscoring

the critical role of energy-aware design in UAV-based communication networks. Our results elucidated an optimal number of reflective elements for the RIS and antennas for the FDR, precisely tailored to the studied scenario, with our optimization algorithm suggesting a possible reduction in the optimal number of reflective elements. The analysis showed that increasing the number of reflective elements for the RIS logarithmically improves the rate for each GN, but also increases the energy consumption due to the added weight, which represents a tradeoff between channel gain and energy efficiency. Despite the nearly passive nature of the RIS, its significant weight, coupled with the inherent double path loss, challenges its applicability in the considered scenario. In contrast, the FDR was consistently identified as a more efficient solution, optimizing network fairness through its favorable path loss without significantly impacting the UAV's energy consumption. Furthermore, the primary energy consumption factor was identified as the UAV's motors, highlighting the importance of lightweight design, especially for UAV-mounted RIS systems. Finally, it was shown that the UAV's battery energy significantly influences the optimal trajectory, forcing the UAV to move only when necessary to minimize energy consumption, thus emphasizing the importance of energy awareness in the strategic operation of UAV-assisted networks. Therefore, our study lays the foundation for future exploration of advanced RIS technologies, e.g., metasurface-based RIS and nonorthogonal multiple access schemes, which promise to unravel complex dynamics and further improve the efficiency and sustainability of UAV-assisted communication networks.

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